

Upper Bound on Transducer and Radiation Efficiencies of a Multi-port Antenna Array

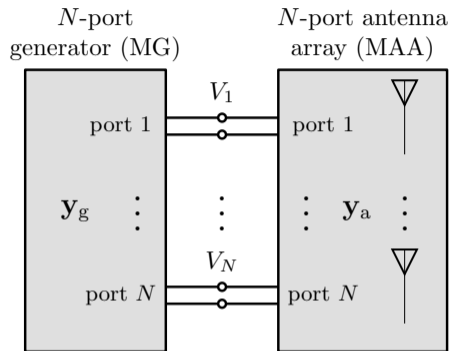
Miloslav Čapek and Lukáš Jelínek

Department of Electromagnetic Field
Czech Technical University in Prague
Czech Republic

miloslav.capek@fel.cvut.cz

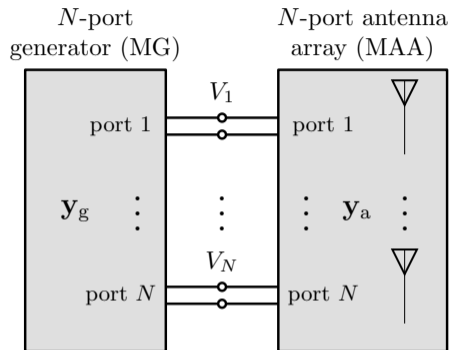
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The goal is to determine the performance limits of multi-port antennas (MAA) in terms of efficiency¹.



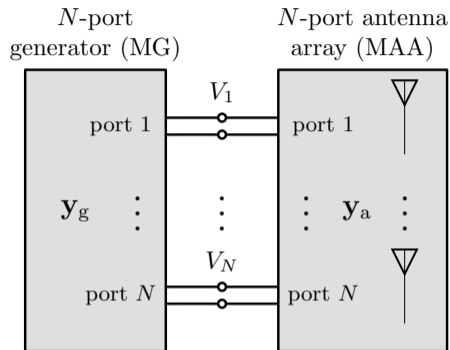
The goal is to determine the performance limits of multi-port antennas (MAA) in terms of efficiency¹.

- ▶ How to define (total) efficiency?
- ▶ How to cope with (ohmic) losses?
- ▶ How much do we know about excitation?



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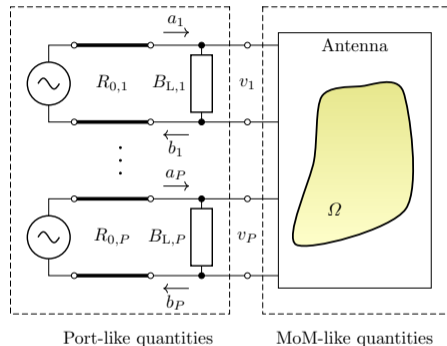
¹M. Capek, L. Jelinek, and M. Masek, “Finding optimal total active reflection coefficient and realized gain for multi-port lossy antennas,” *IEEE Transactions on Antennas and Propagation*, vol. 69, no. 5, pp. 2481–2493, 2021

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Total Active Reflection Coefficient² – Definition

$$\Gamma^t = \sqrt{1 - \frac{P_{\text{rad}}}{P_{\text{in}}}}$$



²M. Manteghi and Y. Rahmat-Samii, “Multiport characteristics of a wide-band cavity backed annular patch antenna for multipolarization operations,” *IEEE Trans. Antennas Propag.*, vol. 53, no. 1, pp. 466–474, 2005.



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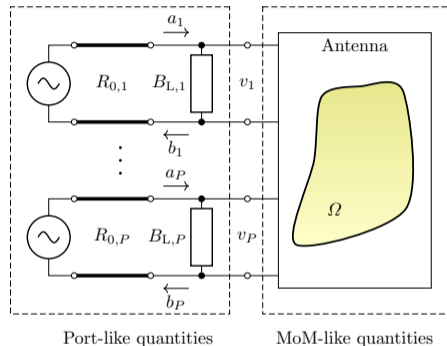
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Radiation and matching efficiencies:

$$\eta_{\text{rad}} = \frac{P_{\text{rad}}}{P_{\text{rad}} + P_{\text{lost}}}$$

$$\eta_{\text{match}} = \frac{P_{\text{rad}} + P_{\text{lost}}}{P_{\text{in}}}$$

$$\eta_{\text{tot}} = \eta_{\text{rad}} \eta_{\text{match}} = 1 - (\Gamma^t)^2$$



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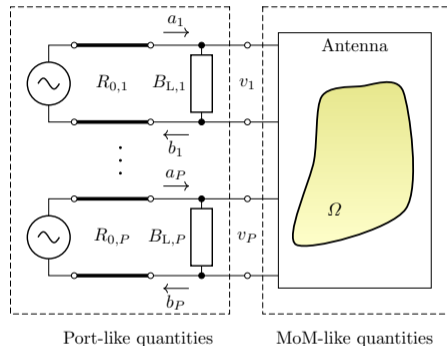
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► Maximizing total efficiency → minimizing TARC.



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Total Efficiency – Optimization

Total efficiency to be maximized (TARC is to be minimized):

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- ▶ How to evaluate P_{in} and P_{rad} ?



Power Terms

Power waves

Total (input) power

$$P_{\text{in}} = \frac{1}{2} \mathbf{a}^H \mathbf{a}.$$

Radiated power

$$P_{\text{rad}} = \frac{1}{2} (\mathbf{a}^H \mathbf{a} - \mathbf{b}^H \mathbf{b}).$$

Reflected power

$$P_{\text{refl}} = \frac{1}{2} \mathbf{b}^H \mathbf{b}.$$



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Method of moments

Total (input) power

$$P_{\text{in}} = P_{\text{rad}} + P_{\text{lost}} + P_{\text{refl}}.$$

Radiated power (always valid)

$$P_{\text{rad}} = \frac{1}{2} \mathbf{I}^H \mathbf{R}_0 \mathbf{I}.$$

Ohmic losses

$$P_{\text{lost}} = \frac{1}{2} \mathbf{I}^H \mathbf{R}_\rho \mathbf{I}.$$



Power Terms in Method of Moments

MoM representation

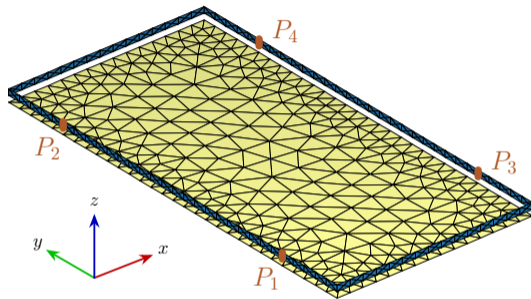
$$\mathbf{J}(\mathbf{r}) \approx \sum_{n=1}^N I_n \psi_n(\mathbf{r})$$

where $\mathbf{I} = [I_n] \in \mathbb{C}^{N \times 1}$ are expansion coefficients gives

$$\mathbf{V} = \mathbf{Z}\mathbf{I}$$

with impedance matrix $\mathbf{Z} \in \mathbb{C}^{N \times N}$ being

$$\mathbf{Z} = \mathbf{R}_0 + \mathbf{R}_\rho + j\mathbf{X}_0.$$





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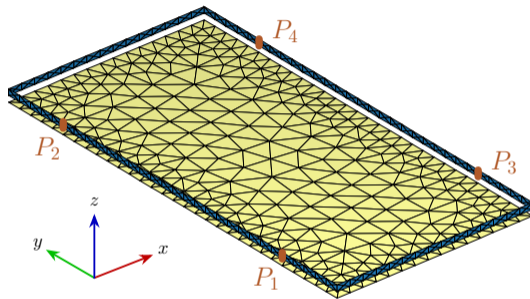
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- We need to express all parameters in terms of port quantities.



Port-mode Representation

Antenna MoM

$$\mathbf{I} = \mathbf{YV}$$

Port MoM

$$\mathbf{i} = \mathbf{y}\mathbf{v}$$



Port-mode Representation

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$$\mathbf{I} = \mathbf{Y}\mathbf{V}$$

Port MoM

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Port-mode excitation

$$\mathbf{V} = \mathbf{C}\mathbf{v}$$

Port current

$$\mathbf{i} = \mathbf{C}^H \mathbf{I}$$



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$\mathbf{C} \in \{0, 1\}^{N \times P}$ is sparse indexing matrix, $\mathbf{C}^H \mathbf{C} = \mathbf{1} \in \mathbb{R}^{P \times P}$ with

$$C_{np} = \begin{cases} 1 & p\text{-th port is placed at } n\text{-th position,} \\ 0 & \text{otherwise.} \end{cases}$$



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Port admittance matrix

$$\mathbf{y} = \mathbf{C}^H \mathbf{Y} \mathbf{C}$$



Port-mode Quantities

The transformation between current and port quantities is generalized as

$$\mathbf{I}^H \mathbf{M} \mathbf{I} = \mathbf{v}^H \mathbf{m} \mathbf{v}$$

for arbitrary \mathbf{M}

$$\mathbf{m} = \mathbf{C}^H \mathbf{Y}^H \mathbf{M} \mathbf{Y} \mathbf{C}.$$

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Port-mode equivalents:

$$P_{\text{rad}} = \frac{1}{2} \mathbf{I}^H \mathbf{R}_0 \mathbf{I} = \frac{1}{2} \mathbf{v}^H \mathbf{g}_0 \mathbf{v}$$

$$P_{\text{lost}} = \frac{1}{2} \mathbf{I}^H \mathbf{R}_\rho \mathbf{I} = \frac{1}{2} \mathbf{v}^H \mathbf{g}_\rho \mathbf{v}$$

$$(\mathbf{Z} = \mathbf{R}_0 + \mathbf{R}_\rho + j\mathbf{X}_0)$$

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Power waves³ ($\mathbf{\Lambda} = \text{diag}(\sqrt{R_{0,p}})$, $\mathbf{y}_L = \text{diag}(jB_{L,p})$)

$$\mathbf{a} = \frac{1}{2} (\mathbf{\Lambda}^{-1} \mathbf{v} + \mathbf{\Lambda} \mathbf{i}) = \mathbf{k}_i \mathbf{v}$$

$$\mathbf{b} = \frac{1}{2} (\mathbf{\Lambda}^{-1} \mathbf{v} - \mathbf{\Lambda} \mathbf{i}) = \mathbf{k}_r \mathbf{v}$$

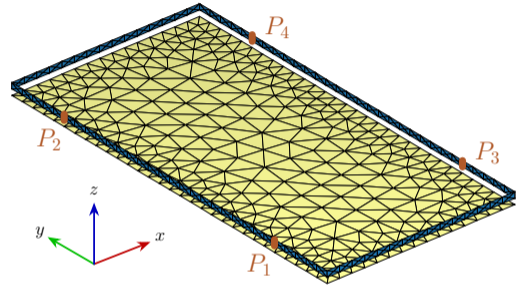
$$(\mathbf{i} = (\mathbf{y} + \mathbf{y}_L) \mathbf{v})$$

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Total Efficiency (TARC) Optimization

$$\begin{aligned} &\text{maximize} && P_{\text{rad}} \\ &\text{subject to} && P_{\text{in}} = 1 \end{aligned}$$



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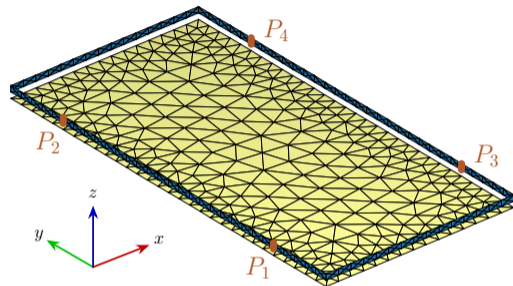


Total Efficiency (TARC) Optimization

$$\begin{aligned} & \text{maximize} && \mathbf{v}^H \mathbf{g}_0 \mathbf{v} \\ & \text{subject to} && \mathbf{v}^H \mathbf{k}_i^H \mathbf{k}_i \mathbf{v} = 1 \end{aligned}$$

Various levels of complexity⁴:

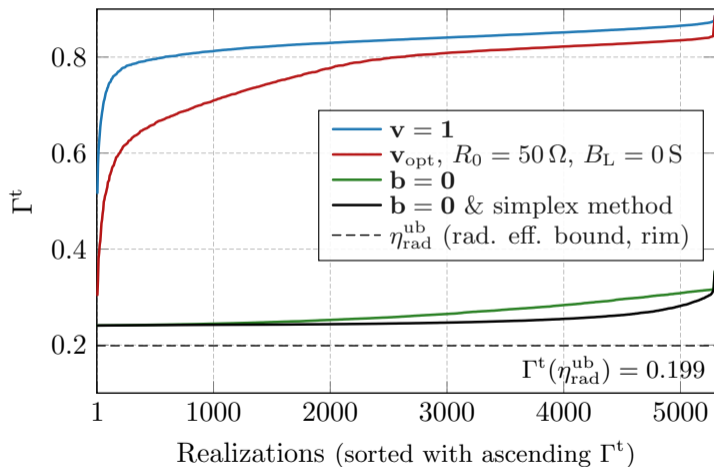
- ▶ optimal excitation of ports,
- ▶ optimal placement of ports,
- ▶ (optimal) number of ports,
- ▶ optimal matching circuitry.



⁴M. Capek, L. Jelinek, and M. Masek, “Finding optimal total active reflection coefficient and realized gain for multi-port lossy antennas,” *IEEE Transactions on Antennas and Propagation*, vol. 69, no. 5, pp. 2481–2493, 2021



Realistic Example – Metallic Rim





Deficiencies (for MIMO)

Knowledge of a multi-port generator

- 1 The approach assumes that MG is known and all its ports are decoupled.
 - ▶ This might not be the case in practice.
 - ▶ Use available power P_{ava} .

$$P_{\text{in}} \longrightarrow P_{\text{ava}}$$



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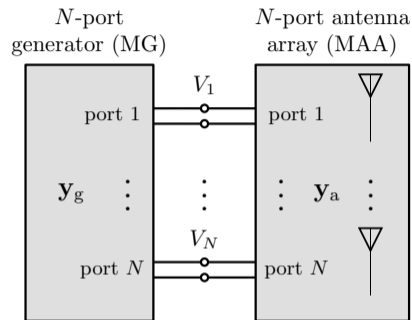
Control of port voltages

- 2 The approach assumes that the optimal voltages are always impressed.
 - ▶ This is not the case of MIMO antennas.
 - ▶ Take care of minimal values as well.

$$\eta_{\text{min}} \leq \eta(\mathbf{v}) \leq \eta_{\text{max}}$$

Available power⁵

Maximum cycle mean power that can be drawn from the generator by an arbitrary LTI and passive load.



⁵C. Desoer, "The maximum power transfer theorem for n-ports," *IEEE Transactions on Circuit Theory*, vol. 20, no. 3, pp. 328–330, 1973. DOI: [10.1109/TCT.1973.1083664](https://doi.org/10.1109/TCT.1973.1083664)

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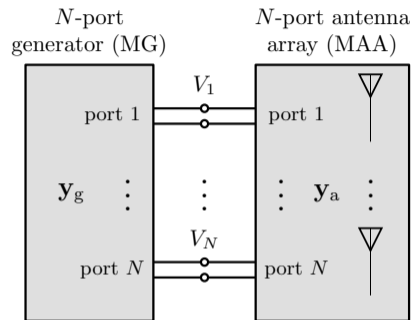
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$$P_{\text{ava}} = \frac{1}{2} \mathbf{v}^H \mathbf{g}_{\text{ava}} \mathbf{v}$$

$$\mathbf{g}_{\text{ava}} = \frac{1}{2} (\mathbf{y}_a + \mathbf{y}_g)^H (\mathbf{y}_g + \mathbf{y}_g^H)^{-1} (\mathbf{y}_a + \mathbf{y}_g)$$



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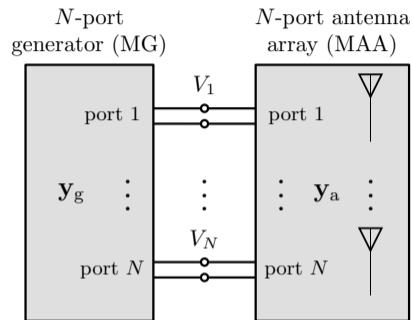
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- Suitable in cases when the internal structure of the generator is complex or not known.



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Approach #2 – Transducer Efficiency



$$\begin{aligned} & \text{maximize/minimize} && \mathbf{v}^H \mathbf{g}_0 \mathbf{v} \\ & \text{subject to} && \mathbf{v}^H \mathbf{g}_{\text{ava}} \mathbf{v} = 1 \end{aligned}$$

solved as

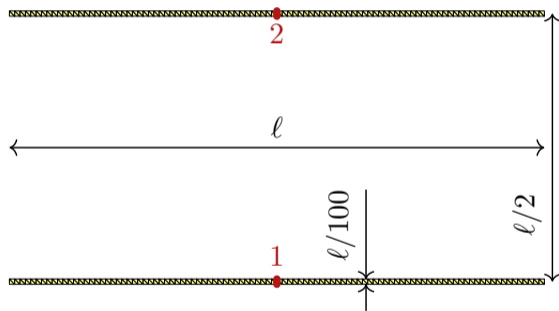
$$\mathbf{g}_0 \mathbf{v}_n = \eta_{T,n} \mathbf{g}_{\text{ava}} \mathbf{v}_n$$

- ▶ Take both the maximum and **minimum** value.

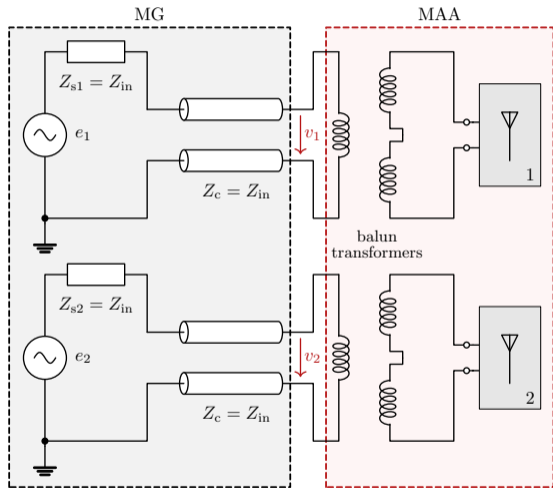


Example

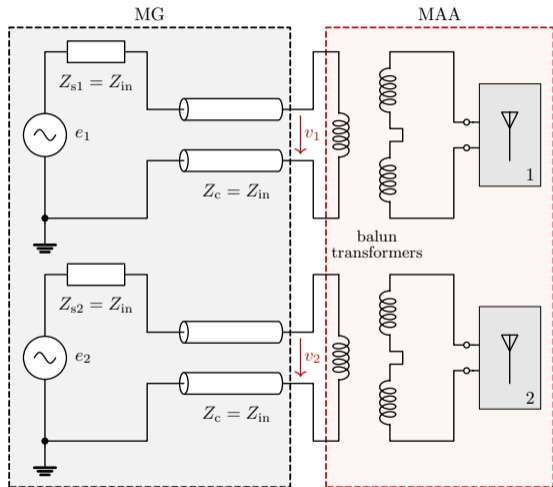
- ▶ Two dipoles, material: copper,
- ▶ $\ell = 187.5$ mm, $f \in [400, 1200]$ MHz,
- ▶ two uncoupled generators, $50\ \Omega$ TML,
- ▶ two Mini-Circuits NCS1.5-232+ RF baluns.



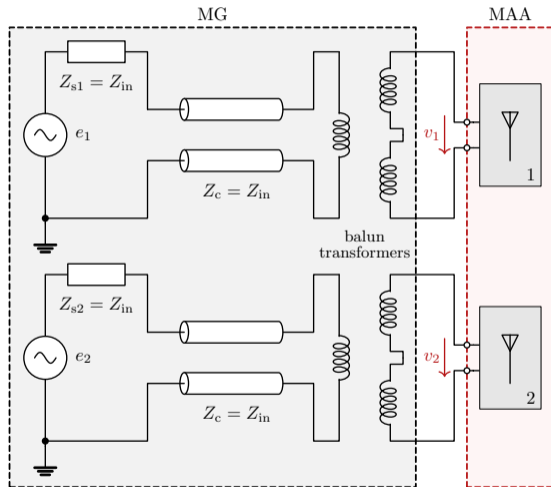
1. MG is known & decoupled (TARC).



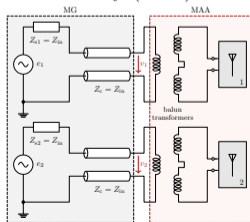
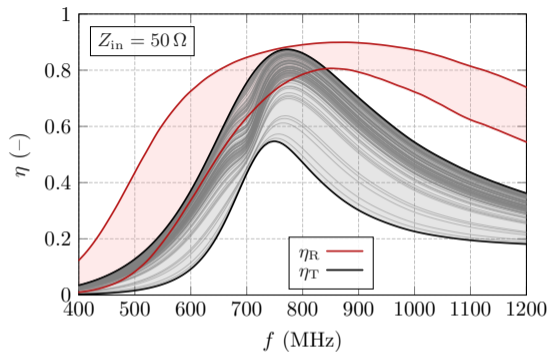
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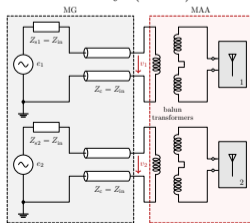
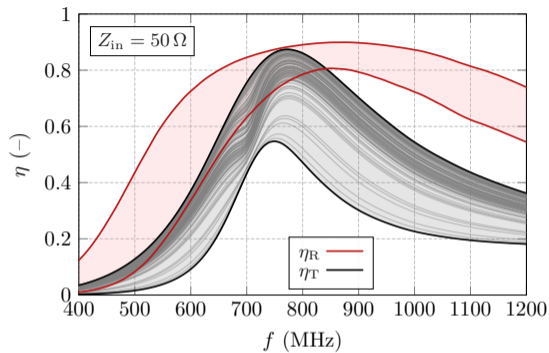
2. MG is unknown (trans. eff.).



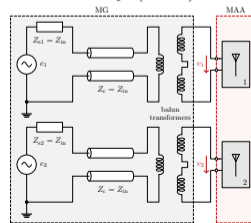
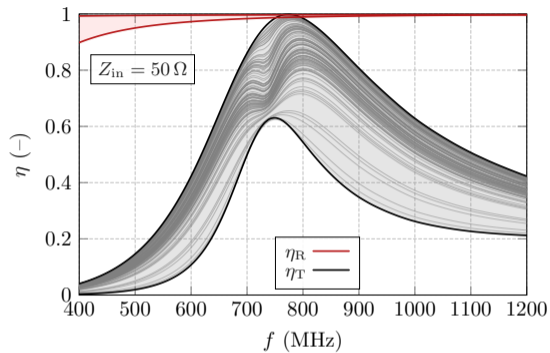
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Conclusion

- ▶ Performance estimates depend on⁶
 - ▶ knowledge about the system,
 - ▶ type of the system to be designed.

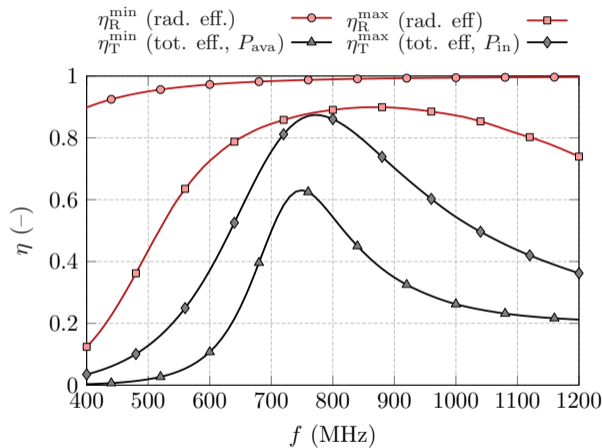
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- ▶ Performance estimates depend on⁶
 - ▶ knowledge about the system,
 - ▶ type of the system to be designed.
- ▶ Use
 - ▶ radiation \times total efficiency,
 - ▶ maximum \times minimum estimates,
 - ▶ input \times available power.

1. MAA (η_R^{\min})
2. \mathbf{y}_g ($\eta_T^{\min}, P_{\text{ava}}$)
3. set \mathbf{v} ($\eta_T^{\max}, P_{\text{ava}}$)
4. MG (η_R^{\max})
5. set \mathbf{v} & matching ($\eta_T^{\max}, P_{\text{in}}$)



⁶M. Capek and L. Jelinek, “Transducer and radiation efficiency figures of a multiport antenna array,” *IEEE Trans. Antennas Propag.*, vol. 71, no. 7, pp. 6132–6137, Jul. 2023

Questions?

Miloslav Čapek
`miloslav.capek@fel.cvut.cz`

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version 1.0

The presentation is available at

▶ capek.elmag.org

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